



Liquidus Projection of the Al-Ta-V System

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Abstract Phase equilibria in the Al-Ta-V system have an important role for designing Al-containing refractory multiprincipal element alloys. In order to improve the available data related to this system and contribute to the development of alloys with good microstructural stability and oxidation resistance, the *liquidus* projection of the Al-Ta-V system is reported for the first time in the present work. The experimental investigations were carried out via microstructural characterization of thirty-one as-cast alloys using scanning electron microscopy (SEM), energy dispersive spectroscopy (EDS) and x-ray diffractometry (XRD). The primary solidification field of BCC is preponderant in relation to those of the other phases. No microstructural signs of phase separation were observed between the isostructural VAl_3 and (ϵ)-

TaAl_3 phases, which suggest a MeAl_3 solid solution connecting the Al-Ta and Al-V binary edges. Alloys in all of the primary solidification fields up to 85 at. % (BCC, σ , $\text{Ta}_{39}\text{Al}_{69}$, V_5Al_8 , MeAl_3) were experimentally produced. Two class II and one type III ternary invariant reactions are suggested based on experimental data: $(\text{U}_I) \text{Liq} + \sigma \leftrightarrow \text{BCC} + \text{Ta}_{39}\text{Al}_{69}$, $(\text{U}_{II}) \text{Liq} + \text{Ta}_{39}\text{Al}_{69} \leftrightarrow \text{V}_5\text{Al}_8 + \text{MeAl}_3$ and $(\text{P}_I) \text{Liq} + \text{BCC} + \text{V}_5\text{Al}_8 \leftrightarrow \text{Ta}_{39}\text{Al}_{69}$. Ternary invariant reactions near to the Al-rich corner are suggested based on extrapolated thermodynamic data. The reported ternary compound $\tau\text{-Al}_{35-48}\text{Ta}_{32-42}\text{V}_{17-30}$ was not observed in the microstructures of the as-cast alloys obtained in the present work, suggesting that its formation occurs from a solid-state reaction.

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1 Introduction

Multiprincipal element alloys (MEAs), also called high entropy alloys (HEAs) are potential materials to be used as structural components at high temperature applications, especially those constituted by refractory metals.^[1,2] In this context, several research groups are investigating refractory multiprincipal element alloys (RMEAs) with Al addition, in order to obtain low density alloys with good oxidation resistance.^[3–6] In this context, the study of the phase equilibria in ternary systems involving refractory metals and Al is important,^[7–11] since the use of these data, along with thermodynamic information and computational tools allows the design of alloys with single-phase

microstructures.^[12–15] Considering the multicomponent system Al–Cr–Nb–Ta–Ti–V–Zr, a careful review of the literature indicated some ternary subsystems with little or no information available, such as the Al–Ta–V system, for which no *liquidus* projection had been reported until now. In the present work, the experimental *liquidus* projection for the Al–Ta–V system is reported based on microstructural characterization of thirty-one arc-melted as-cast alloys.

2 Literature Review

2.1 Binary Systems

The Al–V system was experimentally investigated by several authors^[16–19] and the results reported for this system up to 1989 were summarized by Murray.^[20] Saunders^[21] performed the first thermodynamic assessment of this system. More recently, a paper published by Richter and Ipsen^[22] presented an enhanced version of the aluminum rich part of the Al–V system (between 0 and 50 at.% of V). Based on the experimental results obtained from Richter and Ipsen,^[22] three other thermodynamic assessments were performed by Gong et al.,^[23] Lindhal et al.^[24] and Kroupa et al.^[25] Five intermetallic compounds (VAl_3 , V_5Al_8 , V_2Al_{21} , V_4Al_{23} and V_7Al_{45}) are stable in Al–V system, all being formed by peritectic reactions.

Danon and Cervant^[26] performed an assessment to describe the phase equilibria in Ta–V system, using experimental results obtained by Eremenko et al.,^[27] Nefedov et al.^[28] and Savitskii and Efimov.^[29] Danon and Cervant^[26] reported the stability of C14 phase at high temperatures up to 1702K, while the C15 phase is stable up to 1548K. Recently, Pavlů et al.^[30] suggested that the C14 phase can be also stable at lower temperatures based on ab-initio calculations.

The Al–Ta system was calculated by Du and Fetzer^[31] using experimental data from Subramanian et al.^[32] and Mahne et al.^[33] However, the thermodynamic assessment was not consistent with the experimental data obtained by Nowotny and Neckel^[34] on one side, and Meschel and Kleppa^[35] on the other side, which resulted in inconsistent solid state transformations from the calculations.

Recently, Witusiewicz et al.^[36] performed a new thermodynamic assessment using the previous literature data and their own experimental data obtained from heat-treated and as-cast alloys. Three intermetallic compounds (ϵ)– TaAl_3 , σ and $\text{Ta}_{39}\text{Al}_{69}$ are formed from peritectic reactions, while ϕ phase is formed congruently from the σ phase.

Figure 1 shows the most recent thermodynamic assessments of the binary edges associated to the Al–Ta–V

system, calculated with the thermodynamic parameters from Kroupa et al.^[25] for the Al–V system; Pavlů et al.^[30] for the Ta–V system and Witusiewicz et al.^[36] for the Al–Ta system. These calculated phase diagrams were used to support the analysis and customize the figures and tables of the present work. The crystallographic data^[37] of the stable phases are presented in Table 1 and the invariant reactions from the binary systems are found in Table 2.

2.2 Al–Ta–V Ternary System

Raman^[38] reported an experimental isothermal section for the Al–Ta–V system at 1273 K as shown in Fig. 2(a), based on heat-treated samples characterized by x-ray diffraction (XRD). The authors observed a ternary compound, with approximated stoichiometry of Ta_2VAl_3 and a significant range of stability. Bochvar^[39] performed a new evaluation of the phase equilibria reported by Raman,^[38] as shown in Fig. 2(b). Although no additional experimental data was obtained by Bochvar,^[39] the solubility limits of the single-phase regions were better adjusted.

Both authors^[38,39] did not consider the stability of the C15 and ϕ phases on the Ta–V and the Al–Ta sides, respectively, for these isothermal sections at 1273 K, which is inconsistent with the binary systems shown in Fig. 1(b) and (c). Besides that, Raman and Bochvar^[38,39] considered the stability of the Ta_2Al_3 phase, which is inconsistent with the experimental results obtained by Witusiewicz et al.^[36] for the Al–Ta system. Furthermore, phase separation between the isostructural DO_{22} compounds VAl_3 and (ϵ)– TaAl_3 (see Table 1 for more details) was suggested without experimental data. Thus, as far as we know, the phase equilibria in the Al–Ta–V ternary system are not well established.

The composition interval and the crystallographic data of the ternary compound (also called τ – $\text{Al}_{35-48}\text{Ta}_{32-42}\text{V}_{17-30}$) observed by Raman^[38] were recently obtained by Harbrecht et al.^[40] The crystallographic data of this pentagonal antiprismatic columnar structure is indicated with an asterisk symbol in Table 1. These authors indicated that this compound is stable only for temperatures lower than 1473K, forming from BCC in a solid-state reaction.

3 Experimental Procedure

Thirty-one as-cast alloys were prepared from high purity elements Al (min. 99.96 wt.%), Ta (min. 99.8 wt.%) and V (min. 99.7 wt.%). Ingots of 2 g were arc-melted under argon atmosphere (min. 99.995%) in a water-cooled copper crucible. The alloys were melted five times and flipped after each melting step to obtain chemically homogeneous

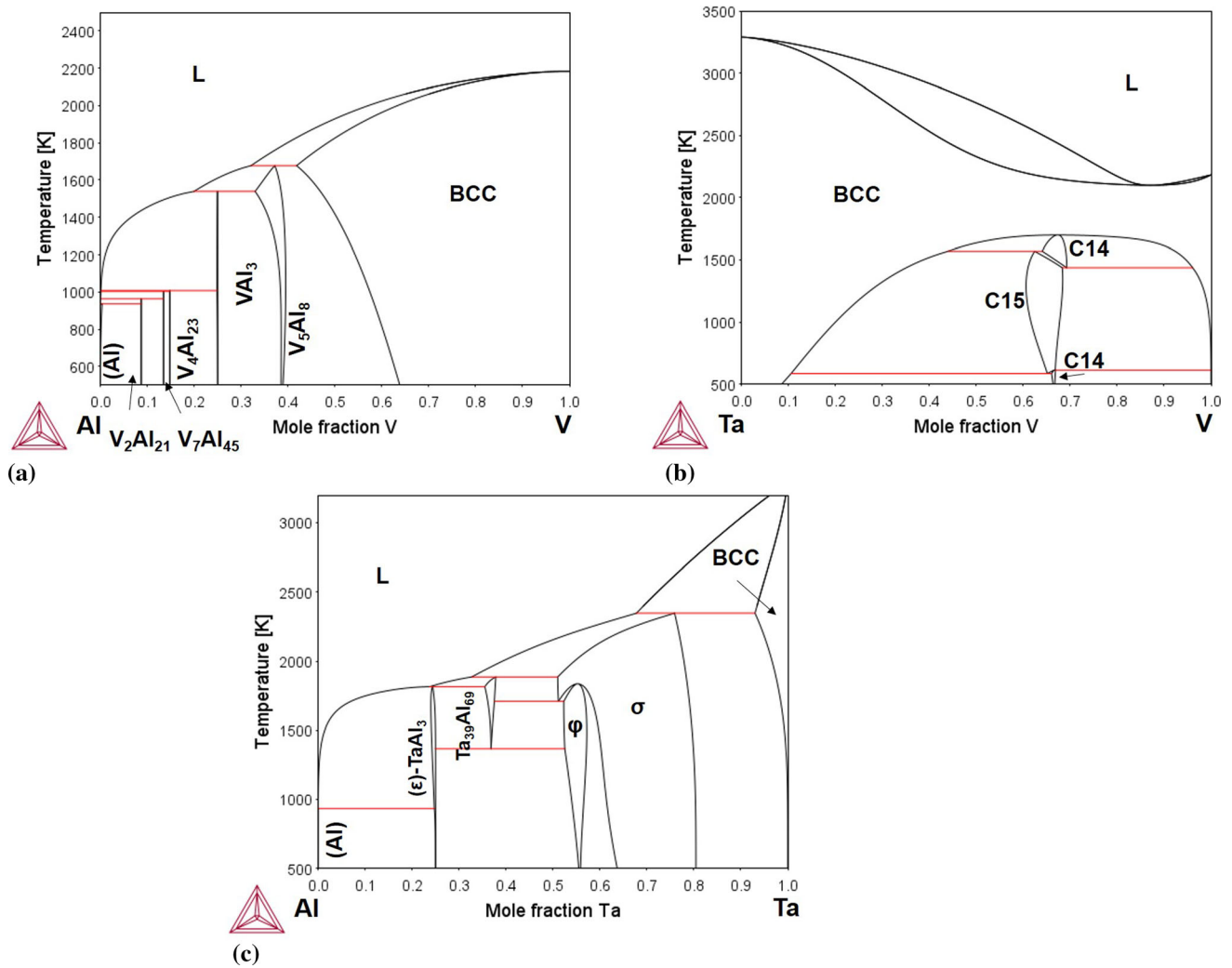


Fig. 1 Binary phase diagrams that composes the Al-Ta-V system: (a) Al-V system,^[25] (b) Ta-V system^[30] and (c) Al-Ta system^[36]

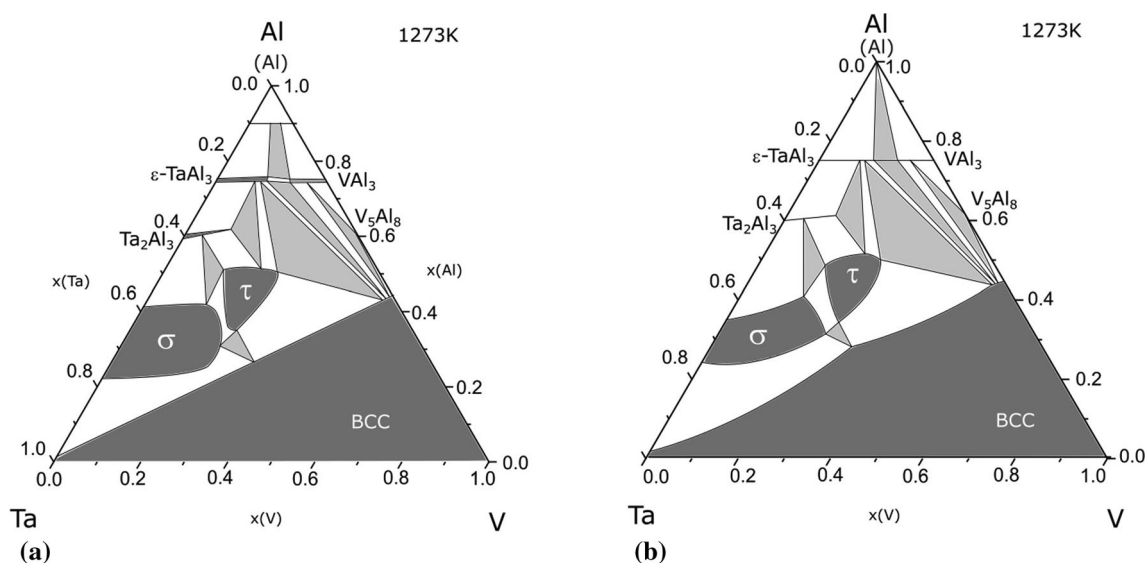
Table 1 Crystallographic data of the solid phases in the Al-Ta-V system^[37]

Phase	Pearson symbol	Space group	Prototype	Strukturbericht designation
(Al)	<i>cF4</i>	<i>Fm</i> $\bar{3}m$	Cu	A1
BCC	<i>cI2</i>	<i>Im</i> $\bar{3}m$	W	A2
V_5Al_8	<i>cI52</i>	<i>I</i> $\bar{4}3m$	Cu_5Zn_8	$D8_2$
VAI_3	<i>tI8</i>	<i>I4/mmm</i>	$TiAl_3$	$D0_{22}$
V_4Al_{23}	<i>hP54</i>	<i>P6_3/mmc</i>	V_4Al_{23}	.
V_7Al_{45}	<i>mC104</i>	<i>C2/m</i>	V_7Al_{45}	.
V_2Al_{21}	<i>cF176</i>	<i>Fd</i> $\bar{3}m$	VAI_{10}	.
σ	<i>tP30</i>	<i>P4_2/mnm</i>	$\sigma\text{-FeCr}$	$D8_b$
ϕ	<i>mP86</i>	<i>P2_1/c</i>	$Ta_{48}Al_{38}$	.
$Ta_{39}Al_{69}$	<i>cF432</i>	<i>F</i> $\bar{4}3m$	$Ta_{39}Al_{69}$	.
$(\epsilon)\text{-TaAl}_3$	<i>tI8</i>	<i>I4/mmm</i>	$TiAl_3$	$D0_{22}$
C14	<i>hP12</i>	<i>P6_3/mmc</i>	$MgZn_2$	C14
C15	<i>cF24</i>	<i>Fd</i> $\bar{3}m$	$MgCu_2$	C15
* $\tau\text{-Al}_{35-48}Ta_{32-42}V_{17-30}$	<i>oC28</i>	<i>Cmca</i>	.	.

*Ternary phase.

Table 2 Invariant reactions involving liquid phase from binary systems^[25,30,36]

Invariant reaction	Identification	Type	Liquid composition	Temp., K	Ref.
Liq. + BCC $\leftrightarrow$ σ	p ¹	Peritectic	75.9 at.% Ta	2347	Al-Ta system ^[36]
Liq. $\leftrightarrow$ BCC	c ¹	Congruent	12.0 at.% Ta	2114	Ta-V system ^[30]
Liq. + $\sigma \leftrightarrow$ Ta ₃₉ Al ₆₉	p ²	Peritectic	37.8 at.% Ta	1885	Al-Ta system ^[36]
Liq. + Ta ₃₉ Al ₆₉ $\leftrightarrow$ (ϵ)-TaAl ₃	p ³	Peritectic	24.4 at.% Ta	1814	Al-Ta system ^[36]
Liq. + BCC $\leftrightarrow$ V ₅ Al ₈	p ⁴	Peritectic	34.8 at.% V	1680	Al-V system ^[25]
Liq. + V ₅ Al ₈ $\leftrightarrow$ VAl ₃	p ⁵	Peritectic	20.5 at.% V	1542	Al-V system ^[25]
Liq. + VAl ₃ $\leftrightarrow$ V ₄ Al ₂₃	p ⁶	Peritectic	< 1.0 at.% V	1009	Al-V system ^[25]
Liq. + V ₄ Al ₂₃ $\leftrightarrow$ V ₇ Al ₄₅	p ⁷	Peritectic	< 1.0 at.% V	1002	Al-V system ^[25]
Liq. + V ₇ Al ₄₅ $\leftrightarrow$ V ₂ Al ₂₁	p ⁸	Peritectic	< 1.0 at.% V	963	Al-V system ^[25]
Liq. + V ₂ Al ₂₁ $\leftrightarrow$ (Al)-FCC	p ⁹	Peritectic	< 1.0 at.% V	936	Al-V system ^[25]
Liq. + (ϵ -TaAl ₃) $\leftrightarrow$ (Al)	p ¹⁰	Peritectic	< 1.0 at.% Ta	933	Al-Ta system ^[36]

**Fig. 2** Isothermal sections of the Al-Ta-V system at 1273 K: (a) Raman^[38] and (b) Bochvar^[39]

samples. Mass losses during the melting process did not exceeded 0.95 wt.%. The metallographic preparation was performed according to the following procedure: the samples were hot-mounted in epoxy resin, ground with SiC abrasive paper (P320 up to P2400), polished with colloidal silica (0.05 μ m), cleaned with ethanol and dried with hot air.

The microstructural characterization of the as-cast alloys was performed using a HITACHI-TM3000 scanning electron microscope (SEM) in the backscattered electrons mode (BSE). The global and the phases chemical compositions were obtained by energy dispersive x-ray spectroscopy (EDS) using a Swift ED-3000 system from Oxford instruments, to guide our microstructural interpretations.

The phases present in each sample were also determined by x-ray diffractometry (XRD) characterization in a

Panalytical Empyrean diffractometer using Cu-k _{α} radiation, scanning angle 2θ in the 10°-90° range with a step size of 0.02° and 50 s counting time. ICSD (Inorganic Crystal Structure Database, 2017) data^[37] were used for interpretation of the powder diffraction patterns. Qualitative and quantitative analyses of the XRD patterns were performed by Rietveld analysis using Topas software (Bruker).

4 Results and Discussion

Table 3 gives the nominal composition of the alloys and their respective mass losses resulting from the arc-melting process. These mass losses did not exceed 1 wt.%, indicating a very small deviation from the nominal

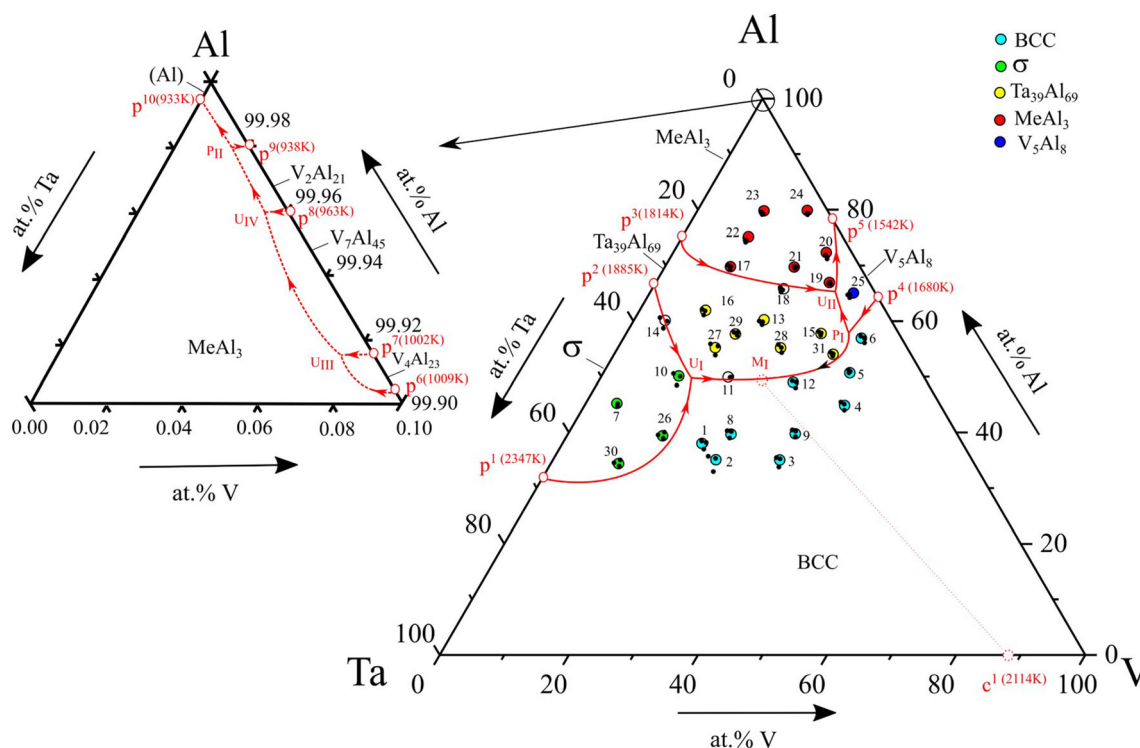
Table 3 Nominal compositions of as-cast alloys and phases identified by SEM/XRD with their respective volume fractions and cell parameters

ID.	Nominal composition			Mass losses wt. %	Possible composition interval			Phase	Vol., %	Cell parameters, Å
	Al, at. %	Ta, at. %	V, at. %		Al, at. %	Ta, at. %	V, at. %			
#1	38.0	40.0	22.0	0.49	36.9-38.3	39.9-40.1	21.3-22.4	BCC*	100.0	$a = 3.1839$
#2	35.0	40.0	25.0	0.91	32.9-35.6	39.7-41.3	23.7-25.8	BCC*	100.0	$a = 3.1775$
#3	35.0	30.0	35.0	0.67	33.7-35.4	29.7-30.6	34.3-35.7	BCC*	100.0	$a = 3.1554$
#4	45.0	15.0	40.0	0.73	44.1-45.4	14.8-15.2	39.5-40.6	BCC*	100.0	$a = 3.1214$
#5	51.0	11.0	38.0	0.06	51.0-51.1	11.0-11.0	37.9-38.0	BCC*	100.0	$a = 3.0504$
#6	57.0	6.0	37.0	0.95	56.3-57.5	5.8-6.1	36.4-37.6	BCC*	31.2	$a = 3.0963$
								V ₅ Al ₈	68.8	$a = 9.2577$
								σ^*	82.8	$a = 9.7643/c = 5.2080$
#7	45.0	50.0	5.0	0.04	45.0-45.1	49.9-50.0	4.9-5.0	Ta ₃₉ Al ₆₉	17.2	$a = 19.1714$
								BCC*	100.0	3.1673
								BCC*	100.0	3.1443
#8	40.0	35.0	25.0	0.51	38.9-40.3	34.9-35.6	24.4-25.5	BCC*	100.0	3.1673
#9	40.0	25.0	35.0	0.52	39.2-40.4	24.8-25.3	34.5-35.5	BCC*	100.0	3.1443
#10	50.0	38.0	12.0	0.84	48.6-50.8	37.7-39.1	10.7-12.3	σ^*	10.5	$a = 9.7756/c = 5.1571$
								BCC	6.0	$a = 3.2989$
								Ta ₃₉ Al ₆₉	59.5	$a = 19.1773$
#11	50.0	30.0	20.0	0.06	49.9-50.1	30.0-30.1	19.9-20.0	BCC	9.4	3.1299
								Ta ₃₉ Al ₆₉	90.6	$a = 19.1313$
								BCC*	100.0	3.1385
#12	48.0	21.0	31.0	0.40	47.1-48.4	20.8-21.3	30.4-31.5	Ta ₃₉ Al ₆₉ (i)*	38.7	$a = 18.7538$
								Ta ₃₉ Al ₆₉ (ii)	22.5	$a = 19.0372$
								BCC	38.8	$a = 3.1249$
#13	60.0	20.0	20.0	0.87	59.6-60.3	19.9-20.2	19.6-20.2	σ^*	10.4	$a = 9.7756/c = 5.0789$
								Ta ₃₉ Al ₆₉	48.3	$a = 19.1744$
								MeAl ₃	41.3	$a = 3.6654/c = 8.3512$
#14	60.0	35.0	5.0	0.26	59.0-60.9	34.7-35.9	3.7-5.1	Ta ₃₉ Al ₆₉ *	100.0	$a = 18.6378$
#15	58.0	12.0	30.0	0.34	57.8-58.1	11.9-12.1	29.8-30.2	Ta ₃₉ Al ₆₉ *	79.4	$a = 19.1303$
#16	65.0	4.0	31.0	0.35	64.8-65.2	3.9-4.0	30.8-31.2	MeAl ₃	20.6	$a = 3.8344/c = 8.4965$
								MeAl ₃ *	57.3	$a = 3.8356/c = 8.5027$
								V ₅ Al ₈	42.7	$a = 9.3169$
#17	70.0	20.0	10.0	0.34	69.6-70.5	19.8-20.3	9.4-10.1	Ta ₃₉ Al ₆₉ *	4.9	$a = 18.6670$
								MeAl ₃	30.3	$a = 3.8224/c = 8.4569$
								V ₅ Al ₈	64.8	$a = 9.3169$
#18	66.0	14.0	20.0	0.35	65.7-66.2	13.9-14.1	19.7-20.2	MeAl ₃ *	57.9	$a = 3.7989/c = 8.3769$
								V ₅ Al ₈	42.1	$a = 9.2673$
								MeAl ₃ *	98.1	$a = 3.7888/c = 8.3507$
#19	72.0	4.0	24.0	0.61	71.8-72.4	3.9-4.0	23.6-24.2	(Al)	1.9	$a = 4.0445$
								MeAl ₃ *	74.0	$a = 3.8115/c = 8.4308$
								V ₅ Al ₈	26.0	$a = 9.2651$
#20	75.0	15.0	10.0	0.15	74.9-75.1	14.9-15.1	9.9-10.0	MeAl ₃ *	100.0	$a = 3.8254/c = 8.4816$
#21	80.0	10.0	10.0	0.22	79.9-80.1	9.9-10.0	9.8-10.0	MeAl ₃ *	93.3	$a = 3.8159/c = 8.4537$
								(Al)	6.6	$a = 4.0449$
								MeAl ₃ *	92.4	$a = 3.7908/c = 8.3628$
#22	80.0	3.0	17.0	0.12	80.0-80.1	3.0-3.0	16.9-17.0	(Al)	7.6	$a = 4.0474$
								V ₅ Al ₈ *	71.4	9.2760
								MeAl ₃	28.6	$a = 3.7918/c = 8.3531$
#23	62.0	28.0	10.0	0.52	61.5-62.5	27.8-28.4	9.4-10.2	σ^*	100.0	$a = 9.7895/c = 5.1139$
#24	40.0	45.0	15.0	0.17	39.8-40.4	44.8-15.1	14.6-15.0	Ta ₃₉ Al ₆₉ (i)*	87.2	$a = 19.1106$
#25	55.0	30.0	15.0	0.64	54.3-55.6	29.7-30.5	14.1-15.2			

Table 3 continued

ID.	Nominal composition			Mass losses wt. %	Possible composition interval			Phase	Vol., %	Cell parameters, Å
	Al, at. %	Ta, at. %	V, at. %		Al, at. %	Ta, at. %	V, at. %			
#28	55.0	20.0	25.0	0.43	54.5-55.2	19.8-20.2	24.7-25.3	Ta ₃₉ Al ₆₉ (ii)	5.7	$a = 18.7041$
								BCC	7.1	$a = 3.1369$
								Ta ₃₉ Al ₆₉ (i)*	9.2	$a = 18.7410$
								Ta ₃₉ Al ₆₉ (ii)	43.2	$a = 19.1067$
#29	57.0	26.0	17.0	0.37	56.6-57.3	25.9-26.2	16.6-17.2	BCC	47.6	$a = 3.1438$
								Ta ₃₉ Al ₆₉ (i)*	79.5	$a = 19.0926$
								Ta ₃₉ Al ₆₉ (ii)	7.2	$a = 18.7680$
#30	35.0	55.0	10.0	0.09	34.9-35.2	54.9-55.1	9.8-10.0	BCC	13.3	$a = 3.1104$
								σ^*	100.0	$a = 9.8141/c = 5.1605$
#31	54.0	12.0	34.0	0.26	53.7-54.1	11.9-12.1	33.9-34.2	Ta ₃₉ Al ₆₉ (i)*	13.1	$a = 18.6247$
								Ta ₃₉ Al ₆₉ (ii)	13.1	$a = 19.0503$
								BCC	73.8	$a = 3.1163$

*Primary phase.

**Fig. 3** Liquidus projection of Al-Ta-V system reported in this work. The continuous and dashed lines represent the monovariant lines that were determined experimentally or by thermodynamic calculation, respectively [25,30,36]

composition. The possible composition intervals were then calculated by assigning the observed mass loss to each of the elements, resulting in maximum and minimum values, as indicated in Table 3. The observed phases for each alloy are listed, as well as their respective volume fractions and cell parameters obtained from refinement using the

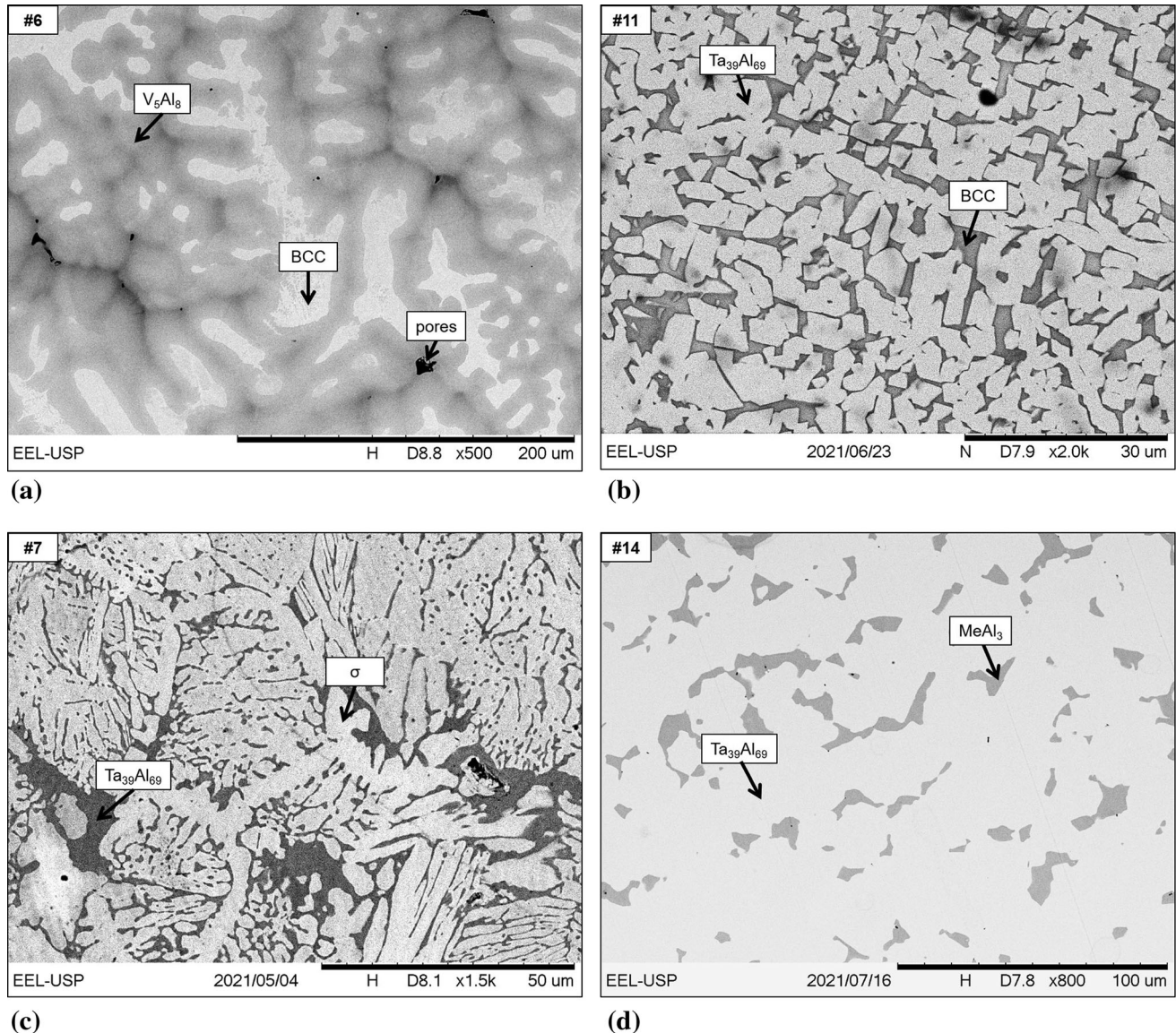
Rietveld analyses. The primary phase is marked with an asterisk symbol.

The experimental liquidus projection reported for the Al-Ta-V system is shown in Fig. 3. The nominal compositions of the samples were plotted using different symbols for the different primary phases identified in each alloy. Three small black circles are also plotted in Fig. 3 denoting

Table 4 Reported ternary invariant reactions of the Al-Ta-V system involving the liquid phase

Ternary invariant reaction	ID	Estimated liquid composition		
		Al, at. %	Ta, at. %	V, at. %
$\text{Liq.} + \sigma \leftrightarrow \text{BCC} + \text{Ta}_{39}\text{Al}_{69}$	U_I	50.0	36.0	14.0
$\text{Liq.} + \text{BCC} + \text{V}_5\text{Al}_8 \leftrightarrow \text{Ta}_{39}\text{Al}_{69}$	P_I	57.0	8.0	35.0
$\text{Liq.} + \text{Ta}_{39}\text{Al}_{69} \leftrightarrow \text{MeAl}_3 + \text{V}_5\text{Al}_8$	U_{II}	66.0	7.0	27.0
$*\text{Liq.} + \text{V}_4\text{Al}_{23} \leftrightarrow \text{MeAl}_3 + \text{V}_5\text{Al}_{47}$	U_{III}	99.92	0.02	0.06
$*\text{Liq.} + \text{V}_7\text{Al}_{45} \leftrightarrow \text{V}_2\text{Al}_{21} + \text{MeAl}_3$	U_{IV}	99.96	0.01	0.02
$*\text{Liq.} + \text{V}_2\text{Al}_{21} + \text{MeAl}_3 \leftrightarrow (\text{Al})$	P_{II}	99.98	0.01	0.01

*Reactions suggested based on extrapolated data from Ref [25, 30, 36]

**Fig. 4** Micrographs (SEM/BSE) of as-cast alloys in the BCC and σ primary solidification fields: (a) #6, (b) #11, (c) #7 and (d) #14

the possible composition deviations for each alloy according to calculations mentioned above. Symbols p^v represent liquid compositions of the peritectic invariant

reactions from the binary systems (see Table 2 for details), while the symbols U, P and M correspond to class II, class III ternary invariant reactions and minimum point,

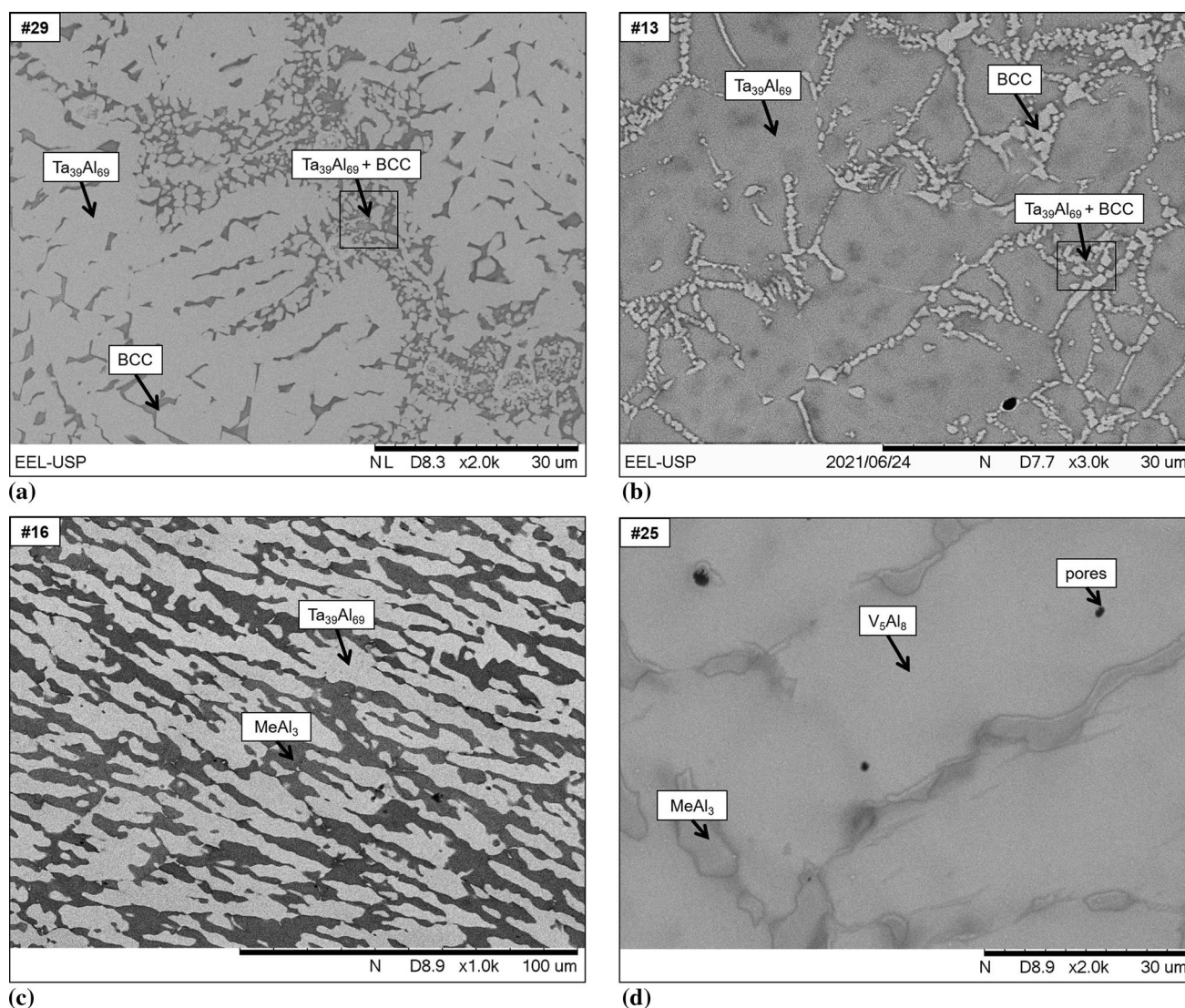


Fig. 5 Micrographs (SEM/BSE) of as-cast alloys in the $Ta_{39}Al_{69}$ and V_5Al_8 primary solidification fields: (a) #29, (b) #13, (c) #16, (d) #25

respectively. The arrows on the monovariant lines indicate the direction of decreasing temperature. The region with Al contents higher than 95 at.% was not investigated due to experimental difficulties. This region is reported based on thermodynamic extrapolation from well-established evaluations of binary subsystems using the Calphad approach.

Microstructural analyses (SEM/BSE, EDS and XRD) of as-cast alloys were used to determine the extents of the primary solidification fields of each phase as well as the nature of the monovariant lines and ternary invariant reactions. Although the isothermal sections at 1273 K reported by Raman and Bochvar^[38,39] suggest an immiscibility of the isostructural compounds VAI_3 and $(\epsilon)\text{-TaAl}_3$, phase separation was not observed in the as-cast microstructures. Thus, the solid solution formed by VAI_3

and $(\epsilon)\text{-TaAl}_3$ in the present investigation is treated here as $MeAl_3$.

Alloys located in the primary solidification fields of BCC , $MeAl_3$, V_5Al_8 , σ and $Ta_{39}Al_{69}$ were produced. BCC primary solidification field is dominant, which is in agreement with its large extent in the binary edges.^[25,30,36] The presence of the ternary compound $\tau\text{-Al}_{35-48}\text{Ta}_{32-42}\text{V}_{17-30}$ was not evidenced in the as-cast alloys, which is in agreement with the results obtained by Harbrecht et al.,^[40] as explained in the section 2.2.

The nature of ternary invariant reactions (four class II and two class III) as well as their liquid phase compositions were estimated taking into consideration the microstructural features of the as-cast alloys and CALPHAD extrapolation based on data from Ref [25, 30, 36] (for

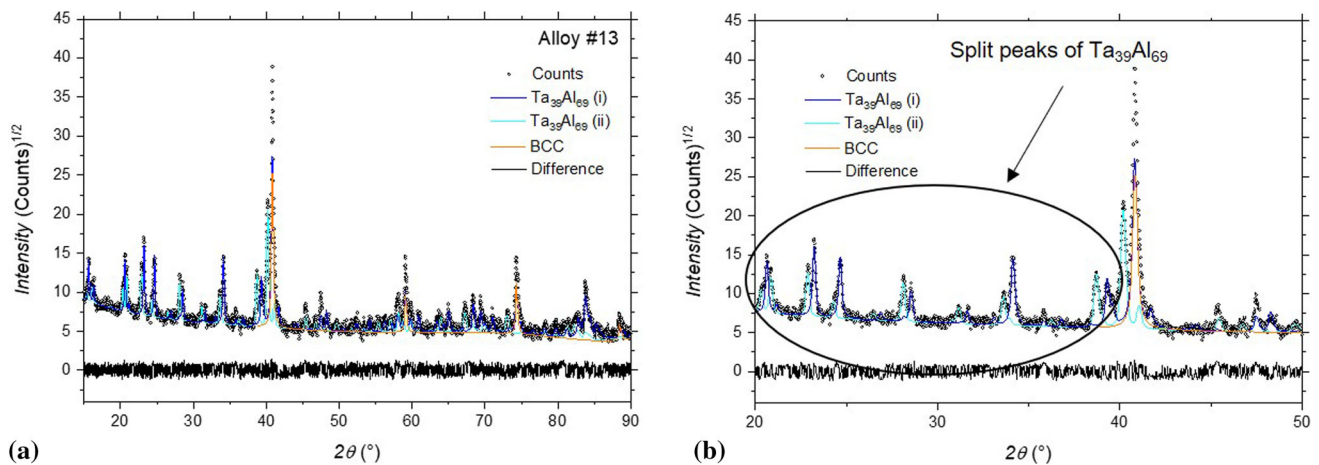


Fig. 6 X-ray diffractograms of as-cast alloy #13 (a) full range (b) details highlighting the split peaks at lower angles

reactions close to the Al corner, indicated in the left side of the Fig. 3).

These reactions are detailed in Table 4. The microstructural features of selected as-cast alloys will be discussed below, grouped in three different regions, to support the *liquidus* projection reported in Fig. 3.

4.1 The Ta-V Rich Region (BCC and σ Primary Solidification Regions)

Primary BCC phase was observed in the SEM/BSE micrographs of alloys #1-#6, #8-#9 and #12. Alloys #1-#5, #8-#9 and #12 solidified as BCC single-phase. No evidence of the ternary compound τ -Al₃₅₋₄₈Ta₃₂₋₄₂V₁₇₋₃₀ was found in the alloys (#1-#4, #8-#9 and #12) located close to its composition range based on the isothermal sections (see Fig. 2).

BCC primary phase surrounded by V₅Al₈ is observed in the SEM/BSE micrograph of alloy #6 shown in Fig. 4(a), suggesting its solidification path towards the p^4 - P_I peritectic-type monovariant line. It is important to mention that V₅Al₈ shows a grey-contrast gradient, associated with the variation of its Al content as a function of temperature, which is consistent with the proposal for this phase in the Al-V system.

Simultaneous solidification of BCC together with Ta₃₉Al₆₉ was observed in the SEM/BSE micrograph of alloy #11, as shown in Fig. 4(b). Considering the morphology of these phases and the results discussed in the next section, the dark-grey regions are the BCC phase, while the polygonal light-grey regions are the Ta₃₉Al₆₉ phase. According to these results, the composition of alloy #11 is placed on the eutectic-type U_I - M_I monovariant line, Fig. 3.

Alloys #26 and #30 solidified as σ single-phase. Fig. 4(c) shows a SEM/BSE micrograph of alloy #7,

containing primary σ phase surrounded by Ta₃₉Al₆₉, which confirms the peritectic nature of the p^2 - U_I monovariant line. The same interpretation was adopted for alloy #10. The SEM/BSE micrograph of alloy #14 indicates only the presence of the Ta₃₉Al₆₉ and MeAl₃ phases, as observed in Fig. 4(d). However, some peaks from σ phase were identified in the XRD analyses, suggesting that its composition is located close to the p^2 - U_I peritectic monovariant line. Thus, two consecutive peritectic reactions are suggested for this alloy composition.

4.2 The Intermediate Region (Ta₃₉Al₆₉ and V₅Al₈ Primary Solidification Regions)

Primary Ta₃₉Al₆₉ phase was observed in the microstructures of alloys #13, #15-#16, #18 and #31. Alloy #15 solidified as Ta₃₉Al₆₉ single-phase.

The SEM/BSE micrographs of alloys #29 and #13 are shown in Fig. 5(a) and (b), respectively. For both alloys, primary Ta₃₉Al₆₉ phase and an eutectic-type microconstituent formed by Ta₃₉Al₆₉ + BCC are observed. The BCC phase has a Ta content smaller than the primary Ta₃₉Al₆₉ phase in alloy #29, while it has a Ta content higher than the primary Ta₃₉Al₆₉ phase in alloy #13. These opposed solidification paths led us to suggest the presence of a minimum point indicated by M_I in Fig. 3, which may be connected to the congruent c^1 point from the Ta-V binary system. Thus, the solidification paths of alloys #27 and #29 move towards the U_I - M_I monovariant line, while the solidification paths of alloys #13, #28 and #31 move towards the P_I - M_I monovariant line. Moreover, split peaks of the Ta₃₉Al₆₉ phase were observed in the XRD results of these group of alloys (#13, #27-#29), which suggest a segregation effect in the Ta₃₉Al₆₉ primary solidification region. These split peaks are shown in the diffractogram of the alloy #13, Fig. 6.

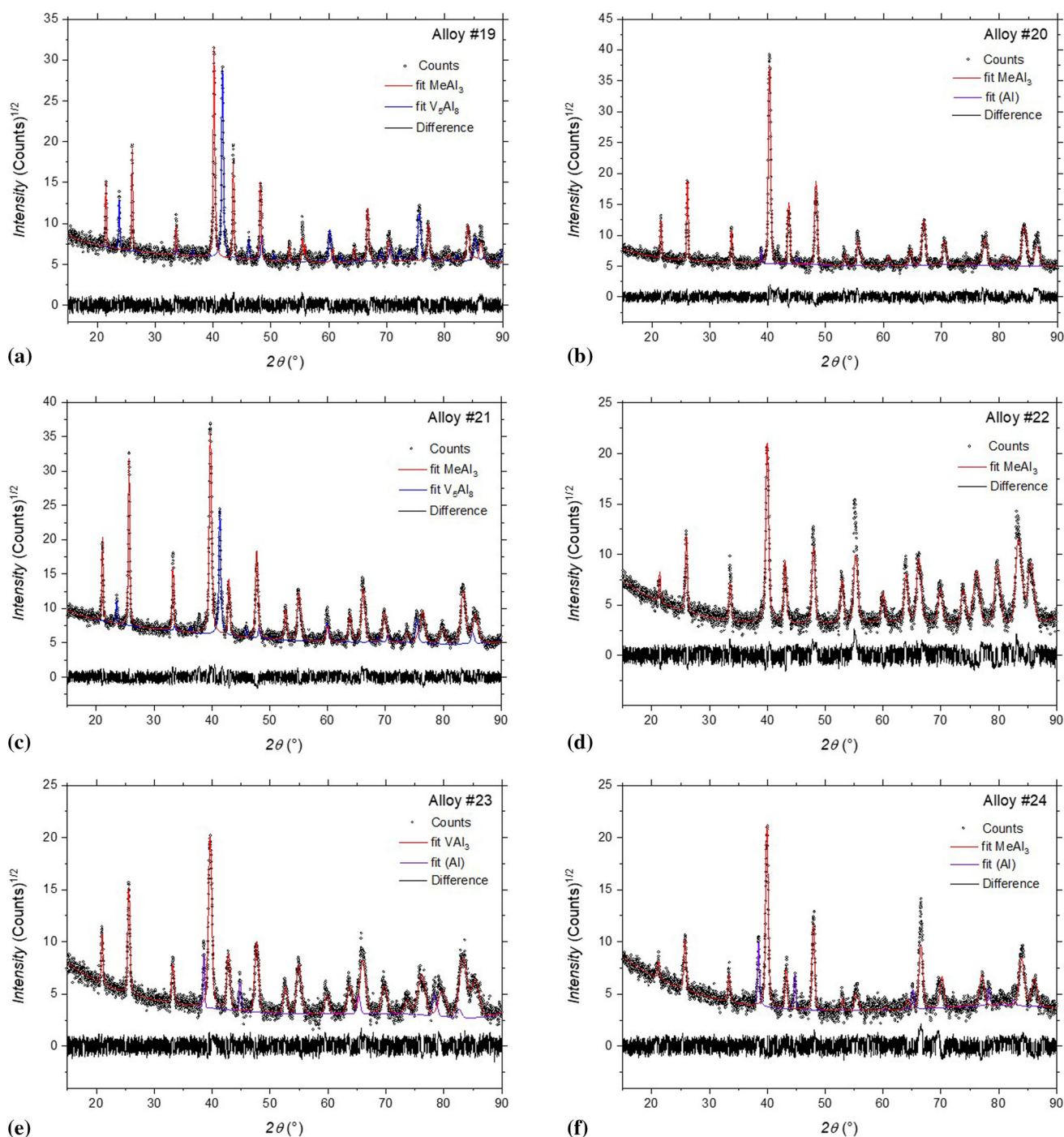


Fig. 7 XRD results of the as-cast alloys in the MeAl_3 primary solidification field: (a) #19, (b) #20, (c) #21, (d) #22, (e) #23 and (f) #24

The SEM/BSE micrograph of alloy #16, Fig. 5(c), shows the primary phase $\text{Ta}_{39}\text{Al}_{69}$ surrounded by MeAl_3 , suggesting a solidification path towards the $\text{p}^3\text{-U}_{II}$ peritectic-type monovariant line.

Some peaks associated with the $\text{Ta}_{39}\text{Al}_{69}$ phase were observed by the XRD analysis of alloy #18, although its presence was not evidenced in the SEM/BSE micrographs.

Furthermore, an eutectic-type microconstituent formed by MeAl_3 and V_5Al_8 was observed in the last solidification region. As discussed above, the $\text{p}^3\text{-U}_{II}$ monovariant line has a peritectic nature, which means that the liquid composition moves from $\text{Ta}_{39}\text{Al}_{69}$ primary solidification field towards the MeAl_3 primary solidification field. In addition, the compound $\text{Ta}_{39}\text{Al}_{69}$ was not observed to the alloys #17,

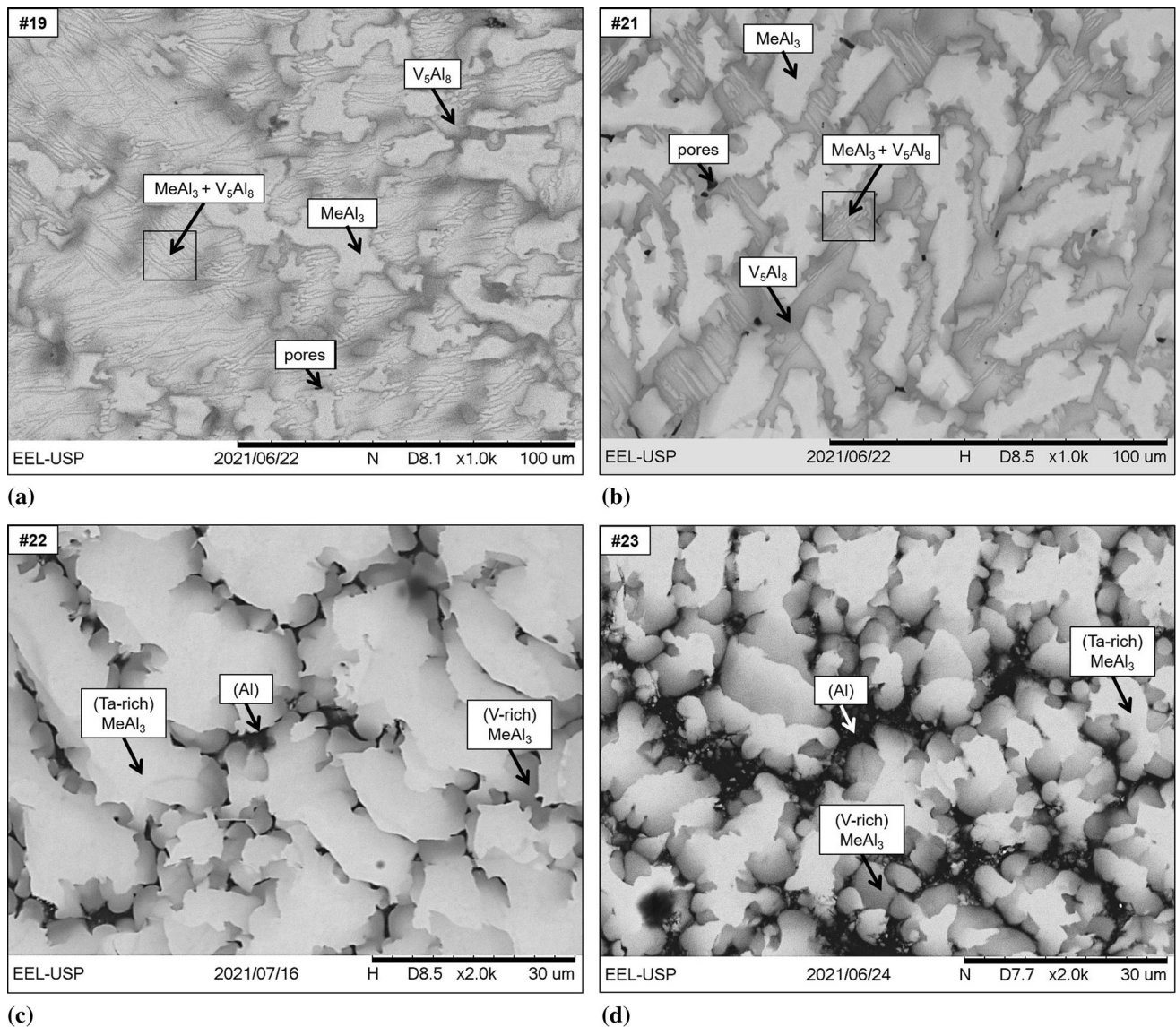


Fig. 8 Micrographs (SEM/BSE) of as-cast alloys in the MeAl_3 primary solidification field: (a) #19, (b) #21, (c) #22 and (d) #23

#19 and #21, which suggest that its composition (alloy #18) is near the $p^3\text{-U}_{II}$ monovariant line.

Fig. 5(d) shows the SEM/BSE micrograph of alloy #25. After the primary solidification of V_5Al_8 , a peritectic formation of MeAl_3 is observed in the last solidification region. Based on the EDS analyses, the MeAl_3 phase has a Ta composition smaller than that of the V_5Al_8 primary phase, suggesting that the solidification moves towards the Al-V binary side. The primary solidification field of V_5Al_8 is restricted to a small region close to the Al-V binary edge, as also observed in the *liquidus* projection of the Al-Nb-V,^[8] which is similar to the present ternary system.

4.3 The Al-rich Corner (MeAl_3 Primary Solidification Region)

Due to experimental difficulties, the *liquidus* projection for Al contents higher than 95 at.% has not been addressed in this work. Therefore, no samples were produced to investigate the primary solidification of V_2Al_{21} , V_7Al_{45} and V_4Al_{23} phases. The construction indicated with dashed lines in Fig. 3 is tentative for this region (see the insert of Fig. 3 for details). The invariant reactions close to the Al-corner, as well as their compositions are indicated in Table 4, based on thermodynamic extrapolation using data from Ref [25, 30, 36].

Primary MeAl_3 phase was observed in alloys #17 and #19–24. Based on the experimental results obtained from SEM/BSE and XRD (see Fig. 7), no signs of phase separation between VAl_3 and $(\epsilon)\text{-TaAl}_3$ were found.

Fig. 8(a) and (b) show the SEM/BSE micrographs of alloys #19 and #21. An enrichment of V content was observed from the center to the edge of the primary phase, while the Ta content decreased. The liquid composition reaches the $U_{II}\text{-p}^5$ monovariant line, when a eutectic-type microconstituent (formed by MeAl_3 and V_5Al_8) is solidified. In addition, the remaining liquid was transformed into V_5Al_8 . The same solidification path was observed for the alloy #17. Comparing the solidification paths of these alloys with the microstructural data obtained for alloy #25, it is possible to suggest a change of nature of the $U_{II}\text{-p}^5$ monovariant line, (i.e. eutectic-type microstructures are solidified for compositions close to U_{II} , while peritectic-type microstructures are solidified for compositions close to p^5). The transition of the nature in the $U_{II}\text{-p}^5$ may be placed between the compositions indicated by #19 and #20 in Fig. 3. This behavior was also observed in the *liquidus* projection of the Al-Nb-V^[8] from the monovariant line between the MeAl_3 and V_5Al_8 primary solidification fields. Furthermore, the possible hypotheses of the presence of a maximum point at the $U_{II}\text{-p}^5$ is not consistent, since no sign of a class I reaction was observed in the microstructures of alloys #15, #18 and #19.

Primary MeAl_3 phase followed by peritectic formations of (Al) were observed in SEM/BSE micrographs of alloys #22 and #23, as exemplified in Fig. 8(c) and (d), respectively. The presence of the grey contrast in this primary phase corroborates the assumption of complete solubility in MeAl_3 structure. Moreover, the XRD results for these alloys, presented in Fig. 7, do not show split peaks resulting from the supposed phase separation.

5 Conclusion

Experimental results for the *liquidus* projection for the Al-Ta-V system are presented for the first time in the present work. Based on the microstructural characterization of thirty-one as-cast alloys via SEM/BSE, EDS and XRD, the *liquidus* projection of the Al-Ta-V system is reported. Five primary solidification regions were experimentally identified, with the BCC phase field filling most of the ternary system, as expected by the stability of this phase in the binary systems. The ternary phase $\tau\text{-Al}_{35-48}\text{Ta}_{32-42}\text{V}_{17-30}$ was not found in the as-cast alloys. Two type II and one type III ternary invariant reactions are reported based on the experimental data. For Al contents higher than 99 at.%, two class II and one class III ternary invariant reactions are

suggested based on extrapolated thermodynamic data from binary systems.

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Conflict of interest The authors declare that they have no conflict of interest.

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